

Inversely, the material vector dX is the pull back equivalent of the spatial vector dx , which is expressed as*

$$dX = \phi_*^{-1}[dx] = F^{-1}dx. \quad (4.13)$$

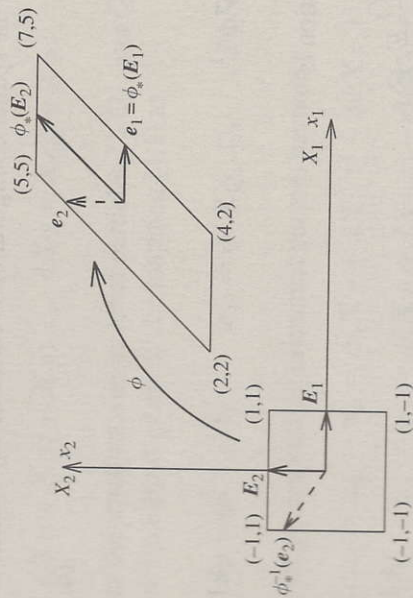
Observe that in (4.12) the nomenclature $\phi_*[\]$ implies an operation that will be evaluated in different ways for different operands [].

EXAMPLE 4.2: Uniform deformation

This example illustrates the role of the deformation gradient tensor F . Consider the uniform deformation given by the mapping

$$\begin{aligned} x_1 &= \frac{1}{4}(18 + 4X_1 + 6X_2); \\ x_2 &= \frac{1}{4}(14 + 6X_2); \end{aligned}$$

which, for a square of side 2 units initially centred at $X = (0, 0)$, produces the deformation shown below.



$$F = \begin{bmatrix} \frac{\partial x_1}{\partial X_1} & \frac{\partial x_1}{\partial X_2} \\ \frac{\partial x_2}{\partial X_1} & \frac{\partial x_2}{\partial X_2} \end{bmatrix} = \frac{1}{2} \begin{bmatrix} 2 & 3 \\ 0 & 3 \end{bmatrix}; \quad F^{-1} = \frac{1}{3} \begin{bmatrix} 3 & -3 \\ 0 & 2 \end{bmatrix}.$$

(continued)

EXAMPLE 4.2: (cont.)

Unit vectors E_1 and E_2 in the initial configuration deform to

$$\phi_*[E_1] = F \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}; \quad \phi_*[E_2] = F \begin{bmatrix} 0 \\ 1 \end{bmatrix} = \begin{bmatrix} 1.5 \\ 1.5 \end{bmatrix};$$

and unit vectors in the current (deformed) configuration deform from

$$\phi_*^{-1}[e_1] = F^{-1} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}; \quad \phi_*^{-1}[e_2] = F^{-1} \begin{bmatrix} 0 \\ 1 \end{bmatrix} = \begin{bmatrix} -1 \\ 2/3 \end{bmatrix}.$$

4.5 STRAIN

As a general measure of deformation, consider the change in the scalar product of the two elemental vectors dX_1 and dX_2 shown in Figure 4.2 as they deform to dx_1 and dx_2 . This change will involve both the stretching (that is, change in length) and changes in the enclosed angle between the two vectors. Recalling Equation (4.7a,b), the spatial scalar product $dx_1 \cdot dx_2$ can be found in terms of the material vectors dX_1 and dX_2 as

$$dx_1 \cdot dx_2 = dX_1 \cdot C dX_2, \quad (4.14)$$

where C is the *right Cauchy–Green deformation tensor*, which is given in terms of the deformation gradient as F as

$$C = F^T F. \quad (4.15)$$

Note that in Equation (4.15) the tensor C operates on the material vectors dX_1 and dX_2 and consequently C is called a material tensor quantity.

Alternatively, the initial material scalar product $dX_1 \cdot dX_2$ can be obtained in terms of the spatial vectors dx_1 and dx_2 via the *left Cauchy–Green* or *Finger tensor* b as*

$$dX_1 \cdot dX_2 = dx_1 \cdot b^{-1} dx_2, \quad (4.16)$$

where b is

$$b = FF^T. \quad (4.17)$$

* In the literature $\phi_*[\]$ and $\phi_*^{-1}[\]$ are often written as ϕ_* and ϕ^* respectively.

* In $C = F^T F$, F is on the right and in $b = FF^T$, F is on the left.

Observe that in Equation (4.16) b^{-1} operates on the spatial vectors $d\mathbf{x}_1$ and $d\mathbf{x}_2$, and consequently b^{-1} , or indeed b itself, is a spatial tensor quantity.

The change in scalar product can now be found in terms of the material vectors $d\mathbf{X}_1$ and $d\mathbf{X}_2$ and the *Lagrangian* or *Green strain tensor* \mathbf{E} as

$$\frac{1}{2}(d\mathbf{x}_1 \cdot d\mathbf{x}_2 - d\mathbf{X}_1 \cdot d\mathbf{X}_2) = d\mathbf{X}_1 \cdot \mathbf{E} d\mathbf{X}_2, \quad (4.18a)$$

where the material tensor \mathbf{E} is

$$\mathbf{E} = \frac{1}{2}(\mathbf{C} - \mathbf{I}). \quad (4.18b)$$

Alternatively, the same change in scalar product can be expressed with reference to the spatial elemental vectors $d\mathbf{x}_1$ and $d\mathbf{x}_2$ and the *Eulerian* or *Almansi strain tensor* \mathbf{e} as

$$\frac{1}{2}(d\mathbf{x}_1 \cdot d\mathbf{x}_2 - d\mathbf{X}_1 \cdot d\mathbf{X}_2) = d\mathbf{x}_1 \cdot \mathbf{e} d\mathbf{x}_2, \quad (4.19a)$$

where the spatial tensor \mathbf{e} is

$$\mathbf{e} = \frac{1}{2}(\mathbf{I} - \mathbf{b}^{-1}). \quad (4.19b)$$

EXAMPLE 4.3: Green and Almansi strain tensors

For the deformation given in Example 4.2 the right and left Cauchy–Green deformation tensors are respectively,

$$\mathbf{C} = \mathbf{F}^T \mathbf{F} = \frac{1}{2} \begin{bmatrix} 2 & 3 \\ 3 & 9 \end{bmatrix} \quad \text{and} \quad \mathbf{b} = \mathbf{F} \mathbf{F}^T = \frac{1}{4} \begin{bmatrix} 13 & 9 \\ 9 & 9 \end{bmatrix},$$

from which the Green's strain tensor is simply

$$\mathbf{E} = \frac{1}{4} \begin{bmatrix} 0 & 3 \\ 3 & 7 \end{bmatrix};$$

and the Almansi strain tensor is,

$$\mathbf{e} = \frac{1}{18} \begin{bmatrix} 0 & 9 \\ 9 & -4 \end{bmatrix}.$$

The physical interpretation of these strain measures will be demonstrated in the next example.

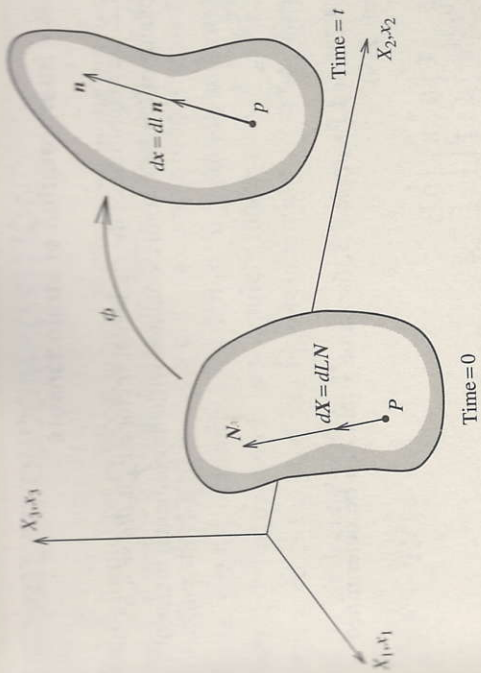


FIGURE 4.3 Change in length.

Remark 4.3: The general nature of the scalar product as a measure of deformation can be clarified by taking $d\mathbf{X}_2$ and $d\mathbf{X}_1$ equal to $d\mathbf{X}$ and consequently $d\mathbf{x}_1 = d\mathbf{x}_2 = d\mathbf{x}$. This enables initial (material) and current (spatial) elemental lengths squared to be determined as (Figure 4.3)

$$dL^2 = d\mathbf{X} \cdot d\mathbf{X}; \quad dl^2 = d\mathbf{x} \cdot d\mathbf{x}. \quad (4.20a,b)$$

The change in the squared lengths that occurs as the body deforms from the initial to the current configuration can now be written in terms of the elemental material vector $d\mathbf{X}$ as

$$\frac{1}{2}(dl^2 - dL^2) = d\mathbf{X} \cdot \mathbf{E} d\mathbf{X}, \quad (4.21)$$

which, upon division by dL^2 , gives the scalar Green's strain as

$$\frac{dl^2 - dL^2}{2 dL^2} = \frac{d\mathbf{X}}{dL} \cdot \mathbf{E} \frac{d\mathbf{X}}{dL}, \quad (4.22)$$

where $d\mathbf{X}/dL$ is a unit material vector \mathbf{N} in the direction of $d\mathbf{X}$, hence, finally

$$\frac{1}{2} \left(\frac{dl^2 - dL^2}{dL^2} \right) = \mathbf{N} \cdot \mathbf{E} \mathbf{N}. \quad (4.23)$$

Using Equation (4.19a), a similar expression involving the Almansi strain tensor can be derived as

$$\frac{1}{2} \left(\frac{dl^2 - dL^2}{dl^2} \right) = \mathbf{n} \cdot \mathbf{e} \mathbf{n}, \quad (4.24)$$

where \mathbf{n} is a unit vector in the direction of $d\mathbf{x}$.

EXAMPLE 4.4: Physical interpretation of strain tensors

Referring to Example 4.2, the magnitude of the elemental vector dx_2 is $dl_2 = 4.5^{1/2}$. Using (4.23), the scalar value of Green's strain associated with the elemental material vector dX_2 is

$$\epsilon_G = \frac{1}{2} \left(\frac{dl^2 - dL^2}{dL^2} \right) = \frac{7}{4}.$$

Again using Equation (4.23) and Example 4.3, the same strain can be determined from Green's strain tensor E as

$$\epsilon_G = N^T E N = [0, 1] \frac{1}{4} \begin{bmatrix} 0 & 3 \\ 3 & 7 \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} = \frac{7}{4}.$$

Using Equation (4.24) the scalar value of the Almansi strain associated with the elemental spatial vector dx_2 is

$$\epsilon_A = \frac{1}{2} \left(\frac{dl^2 - dL^2}{dl^2} \right) = \frac{7}{18}.$$

Alternatively, again using Equation (4.24) and Example 4.3 the same strain is determined from the Almansi strain tensor e as

$$\epsilon_A = n^T e n = \left[\frac{1}{\sqrt{2}}, \frac{1}{\sqrt{2}} \right] \frac{1}{18} \begin{bmatrix} 0 & 9 \\ 9 & -4 \end{bmatrix} \begin{bmatrix} \frac{1}{\sqrt{2}} \\ \frac{1}{\sqrt{2}} \end{bmatrix} = \frac{7}{18}.$$

Remark 4.4: In terms of the language of pull back and push forward, the material and spatial strain measures can be related through the operator ϕ_* . Precisely, how this operator works in this case can be discovered by recognizing, because of their definitions, the equality

$$dx_1 \cdot e \, dx_2 = dX_1 \cdot E \, dX_2 \quad (4.25)$$

for any corresponding pairs of elemental vectors. Recalling Equations (4.12–4.13) enables the push-forward and pull-back operations to be written as

Push forward

$$e = \phi_* [E] = F^{-T} E F^{-1}. \quad (4.26a)$$

Pull back

$$E = \phi_*^{-1}[e] = F^T e F. \quad (4.26b)$$

4.6 POLAR DECOMPOSITION

The deformation gradient tensor F discussed in the previous sections transforms a material vector dX into the corresponding spatial vector dx . The crucial role of F is further disclosed in terms of its decomposition into stretch and rotation components. The use of the physical terminology stretch and rotation will become clearer later. For the moment, from a purely mathematical point of view, the tensor F is expressed as the product of a *rotation tensor* R times a *stretch tensor* U to define the polar decomposition as

$$F = RU. \quad (4.27)$$

For the purpose of evaluating these tensors, recall the definition of the right Cauchy–Green tensor C as

$$C = F^T F = U^T R^T R U. \quad (4.28)$$

Given that R is an orthogonal rotation tensor as defined in Equation (2.26), that is, $R^T R = I$, and choosing U to be a symmetric tensor gives a unique definition of the *material stretch tensor* U in terms of C as

$$U^2 = U U = C. \quad (4.29)$$

In order to actually obtain U from this equation, it is first necessary to evaluate the principal directions of C , denoted here by the eigenvector triad $\{N_1, N_2, N_3\}$ and their corresponding eigenvalues λ_1^2, λ_2^2 , and λ_3^2 , which enable C to be expressed as

$$C = \sum_{\alpha=1}^3 \lambda_\alpha^2 N_\alpha \otimes N_\alpha, \quad (4.30)$$

where, because of the symmetry of C , the triad $\{N_1, N_2, N_3\}$ are orthogonal unit vectors. Combining Equations (4.29) and (4.30), the material stretch tensor U can be easily obtained as

$$U = \sum_{\alpha=1}^3 \lambda_\alpha N_\alpha \otimes N_\alpha. \quad (4.31)$$

Once the stretch tensor U is known, the rotation tensor R can be easily evaluated from Equation (4.27) as $R = F U^{-1}$.

$$\hat{n}_1 = \hat{F}N_1 = \begin{bmatrix} -0.3306 \\ 1.5856 \\ 0 \end{bmatrix}; \quad \hat{n}_2 = \hat{F}N_2 = \begin{bmatrix} -0.8453 \\ -0.1794 \\ 0 \end{bmatrix};$$

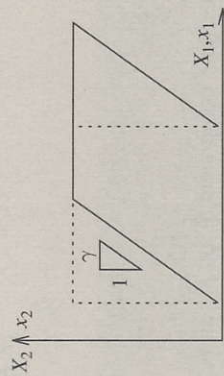
$$\hat{n}_3 = \hat{F}N_3 = \begin{bmatrix} 0 \\ 0 \\ 0.7138 \end{bmatrix}.$$

Since N_α are principal directions, \hat{n}_α are orthogonal vectors and the corresponding elemental spatial volume is conveniently,

$$dv = \|\hat{n}_1\| \|\hat{n}_2\| \|\hat{n}_3\| = 1,$$

thus demonstrating the isochoric nature of \hat{F} .

EXAMPLE 4.8: Simple shear



Sometimes the motion of a body is isochoric and the distortional component of F coincides with F . A well-known example is the simple shear of a two-dimensional block as defined by the motion

$$x_1 = X_1 + \gamma X_2, \\ x_2 = X_2,$$

for any arbitrary value of γ . A simple derivation gives the deformation gradient and its Jacobean J as

$$F = \begin{bmatrix} 1 & \gamma \\ 0 & 1 \end{bmatrix}; \quad J = \det F = 1;$$

and the Lagrangian and Eulerian deformation tensors are

$$E = \frac{1}{2} \begin{bmatrix} 0 & \gamma \\ \gamma & \gamma^2 \end{bmatrix}; \quad e = \frac{1}{2} \begin{bmatrix} 0 & \gamma \\ \gamma & -\gamma^2 \end{bmatrix}.$$

Consider an element of area in the initial configuration $dA = dA N$ which after deformation becomes $da = da n$ as shown in Figure 4.7. For the purpose of obtaining a relationship between these two vectors, consider an arbitrary material vector dL , which after deformation pushes forward to dl . The corresponding initial and current volume elements are

$$dV = dL \cdot dA; \quad (4.66a)$$

$$dv = dl \cdot da. \quad (4.66b)$$

Relating the current and initial volumes in terms of the Jacobian J and recalling that $dl = F dL$ gives

$$J dL \cdot dA = (F dL) \cdot da. \quad (4.67)$$

The fact that the above expression is valid for any vector dL enables the elements of area to be related as

$$da = J F^{-T} dA. \quad (4.68)$$

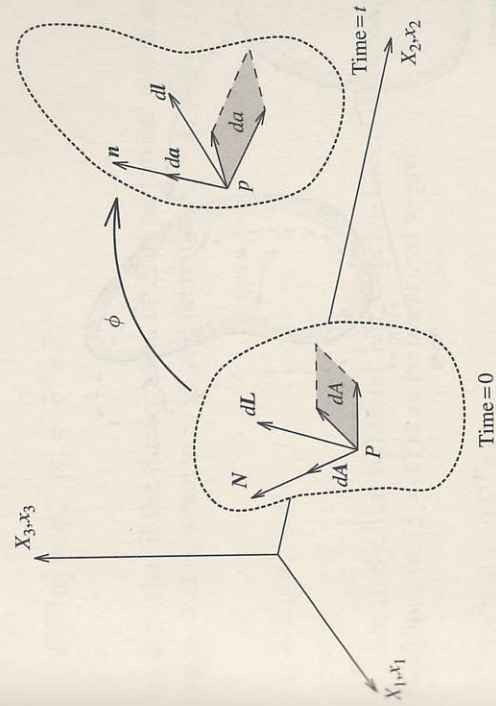


FIGURE 4.7 Area change.