

**Warsaw University
of Technology**



**Faculty of Power and
Aeronautical Engineering**

WARSAW UNIVERSITY OF TECHNOLOGY

Institute of Aeronautics and Applied Mechanics

Finite element method (FEM)

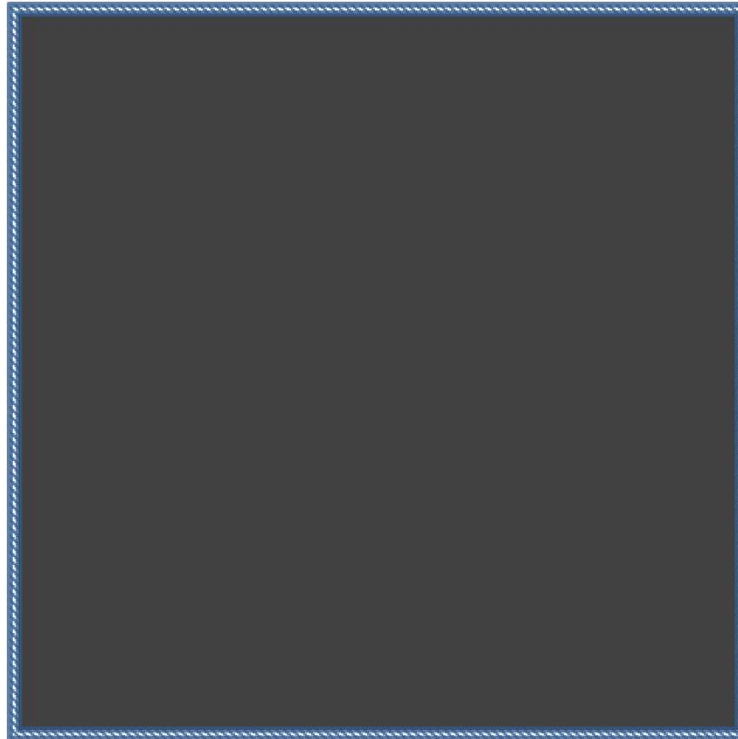
Finite Difference Method. A square plate

06.2021

Square plate

Young's modulus: $E = 2 \cdot 10^5 \text{ MPa}$
thickness: $t = 2 \text{ mm}$

$L = 100 \text{ mm}$

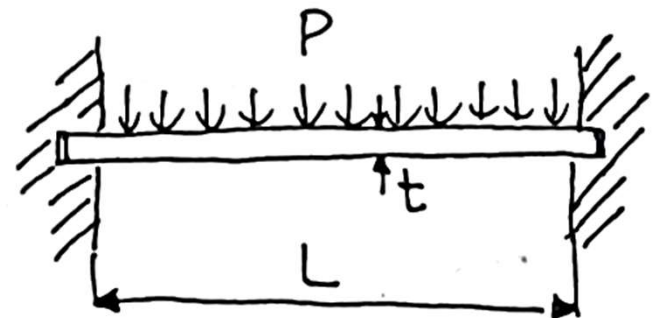


$L = 100 \text{ mm}$

uniform pressure: $p = 0.2 \text{ MPa}$



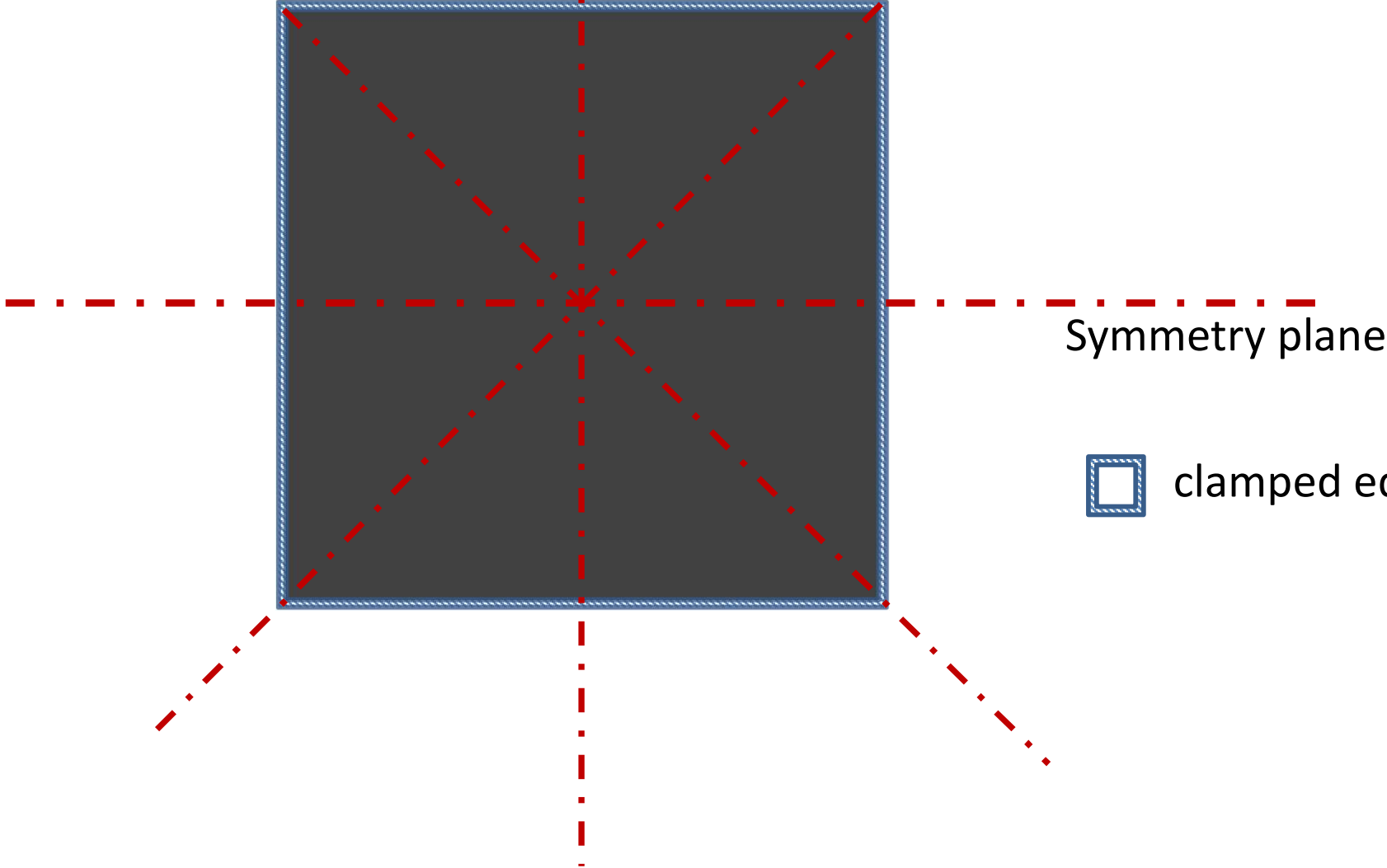
clamped edges



Square plate

Symmetry plane

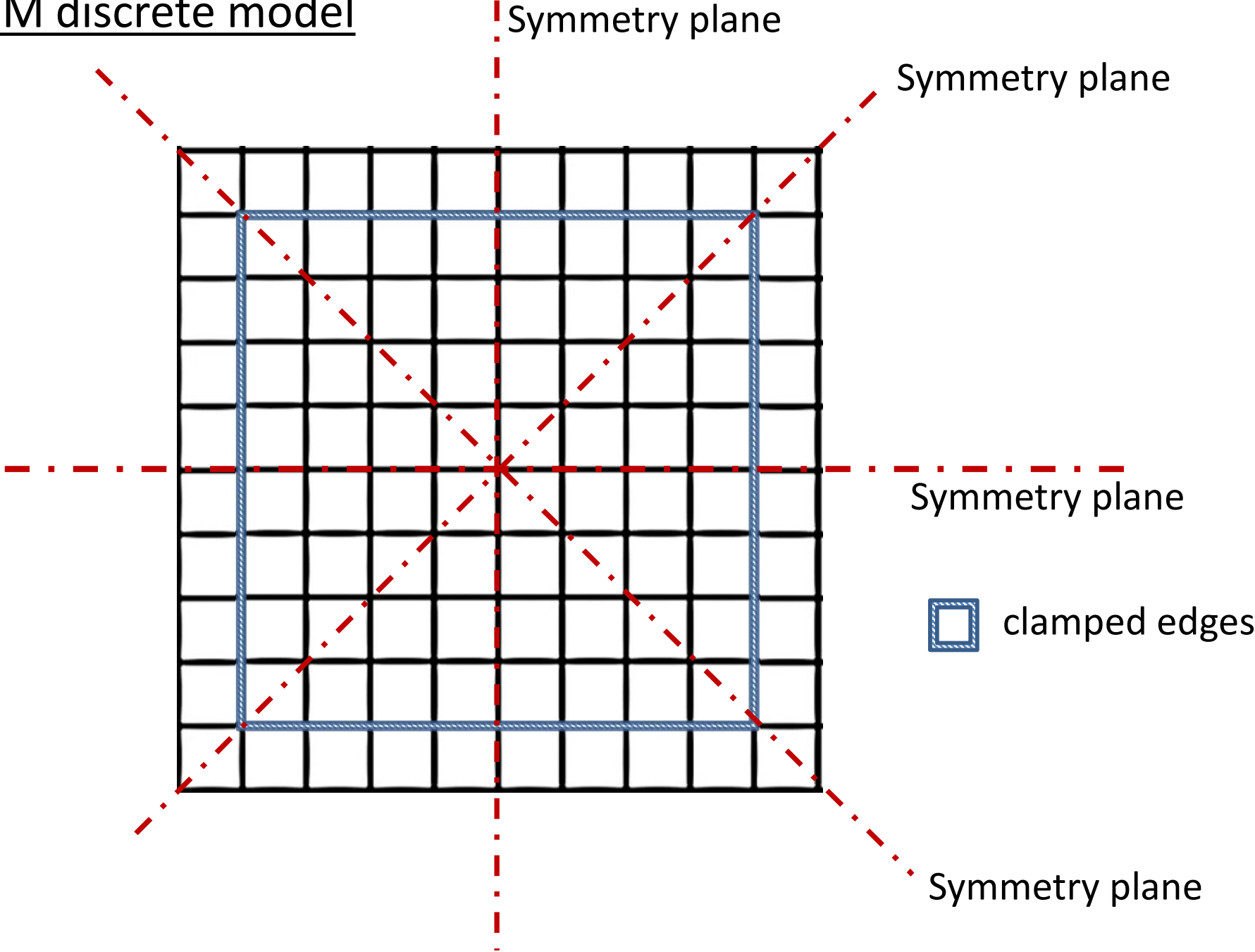
Symmetry plane



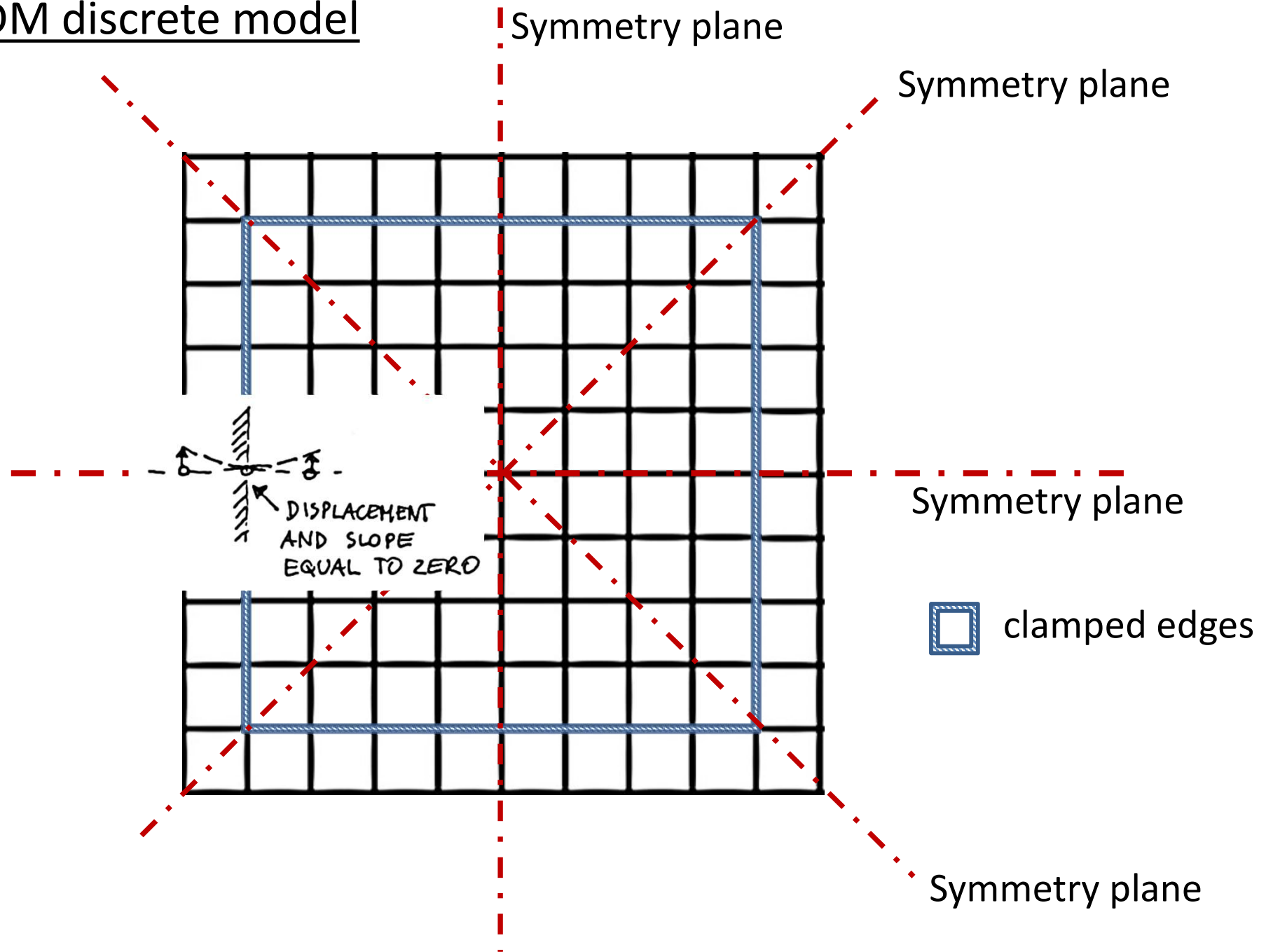
Symmetry plane

 clamped edges

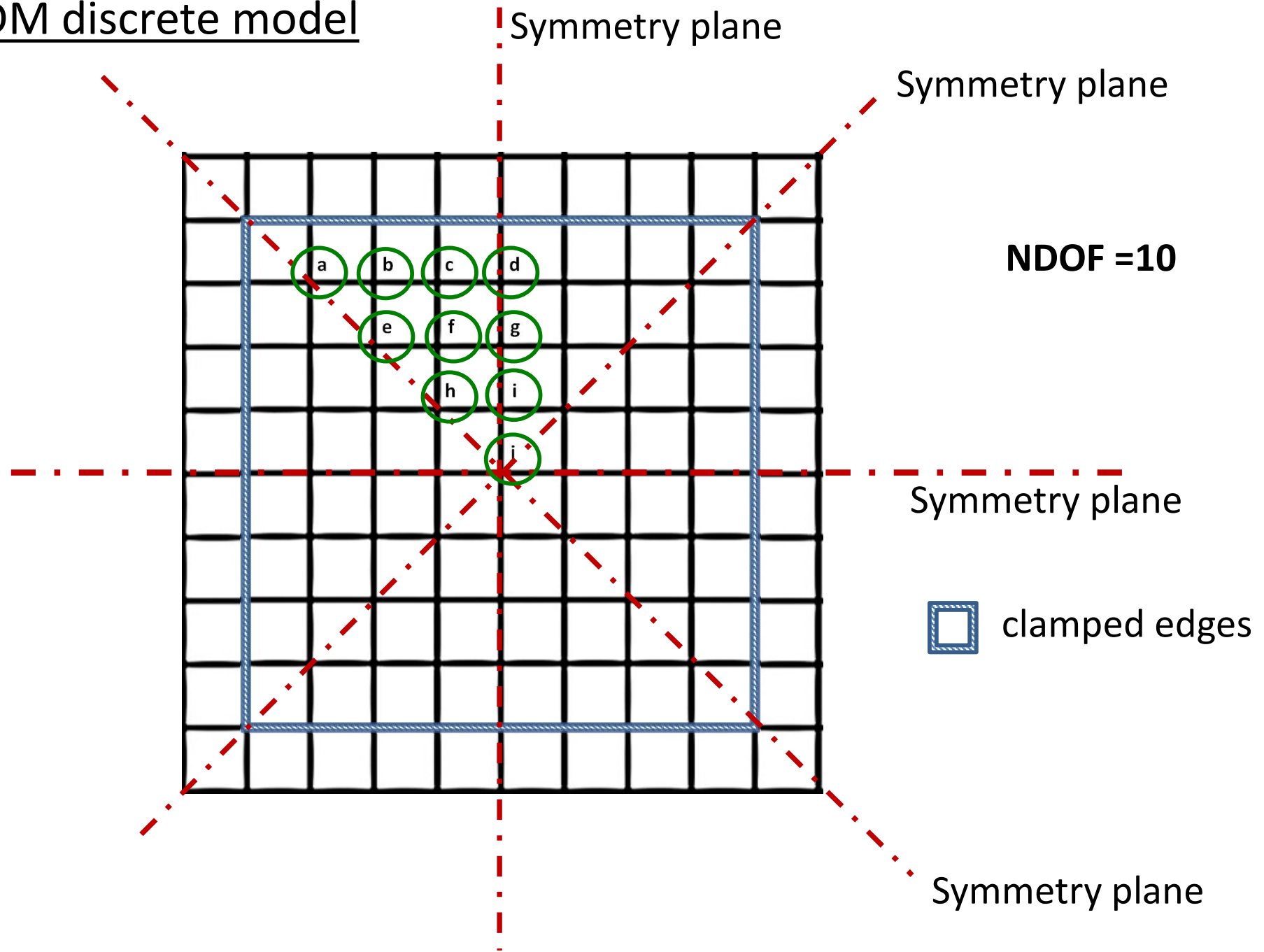
FDM discrete model



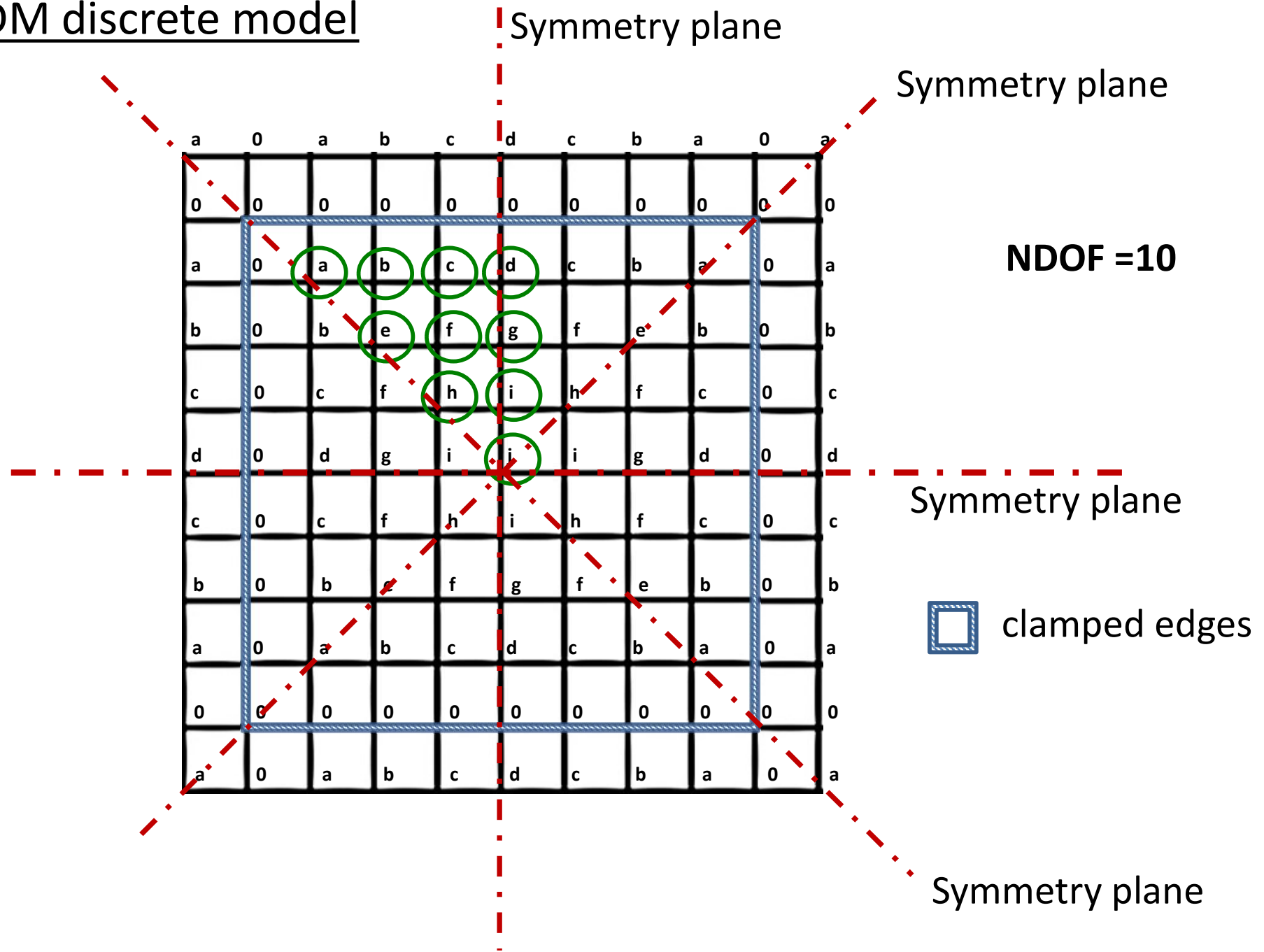
FDM discrete model



FDM discrete model



FDM discrete model



Partial differential equation of a plate:

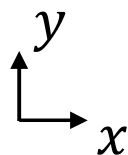
$$\frac{\partial^4 w}{\partial x^4} + 2 \frac{\partial^4 w}{\partial x^2 \partial y^2} + \frac{\partial^4 w}{\partial y^4} = \frac{12p(1 - \nu^2)}{Et^3}$$

$L = 100 \text{ mm}$

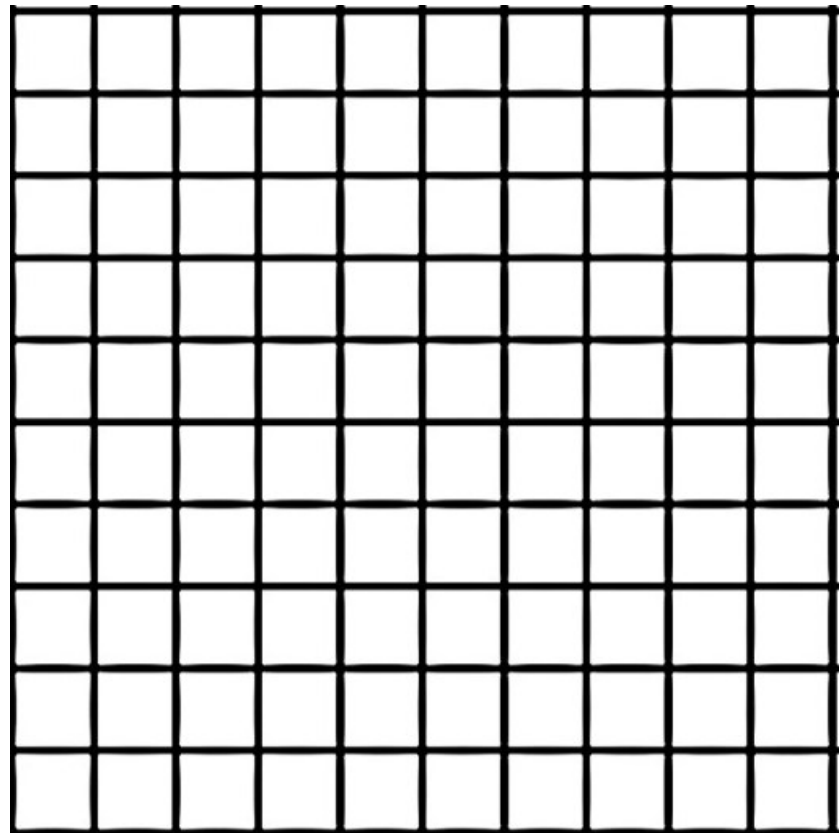
Finite difference equation of a plate:

$$\frac{\Delta^4 w}{\Delta x^4} + 2 \frac{\Delta^4 w}{\Delta x^2 \Delta y^2} + \frac{\Delta^4 w}{\Delta y^4} = \frac{12p(1 - \nu^2)}{Et^3}$$

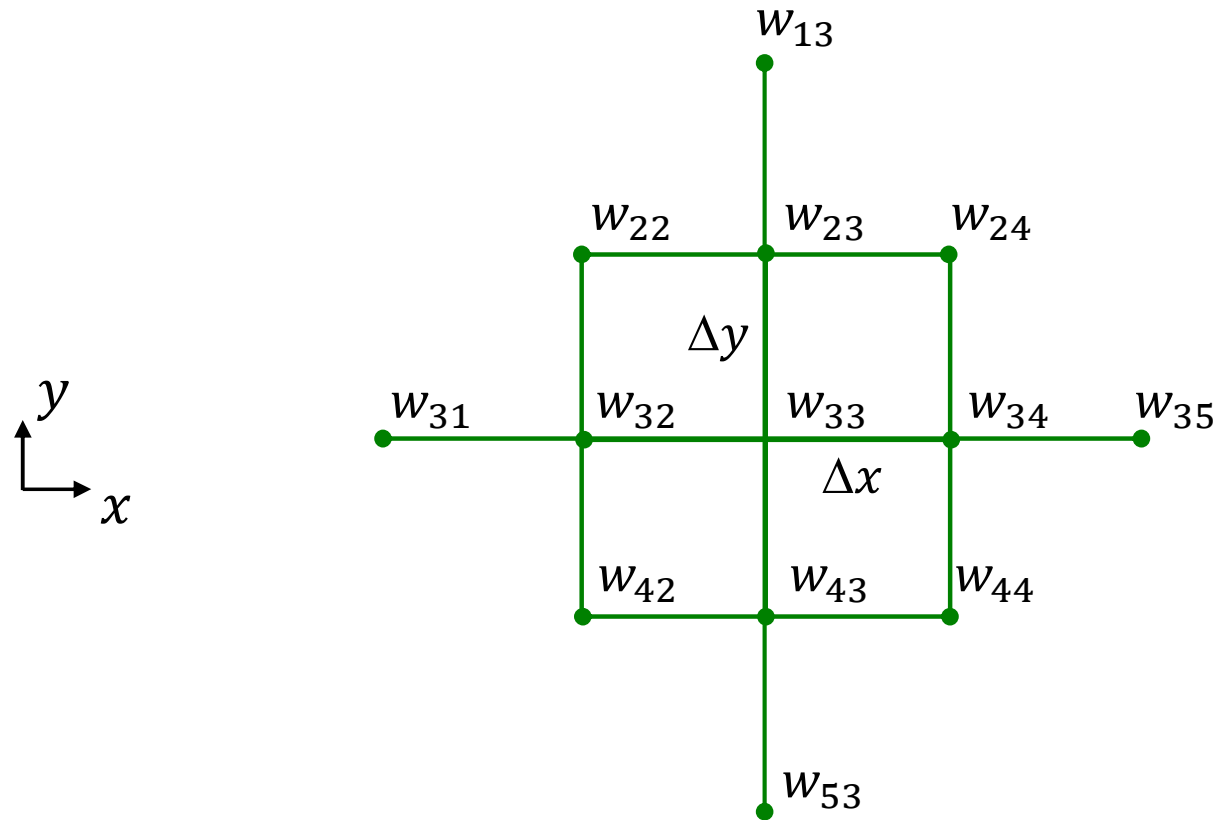
$L = 100 \text{ mm}$



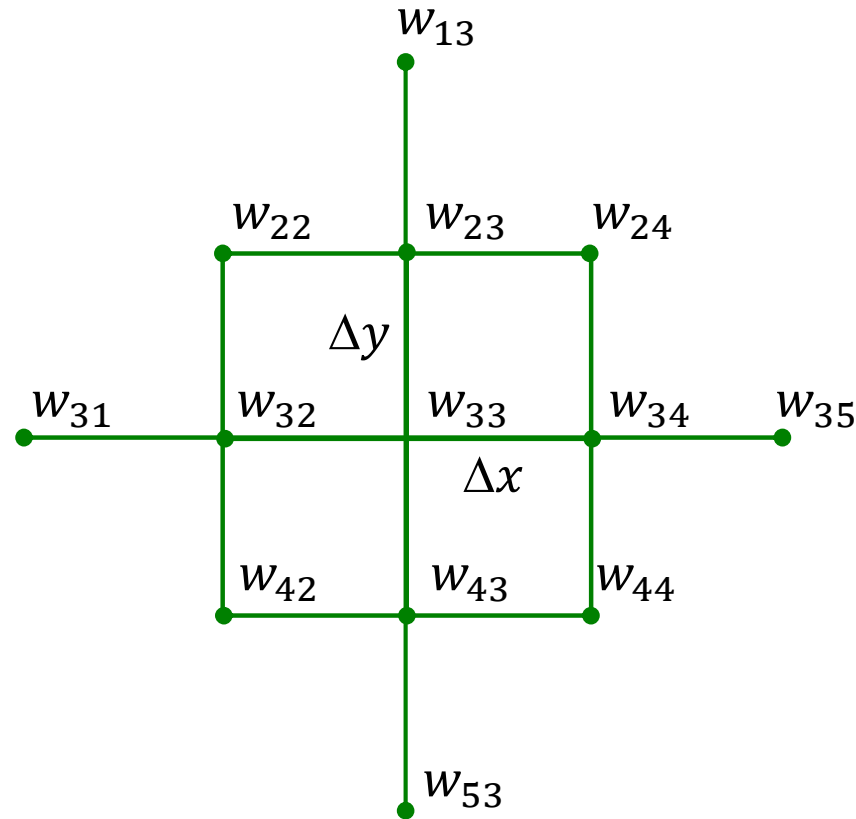
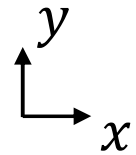
Δy



Δx

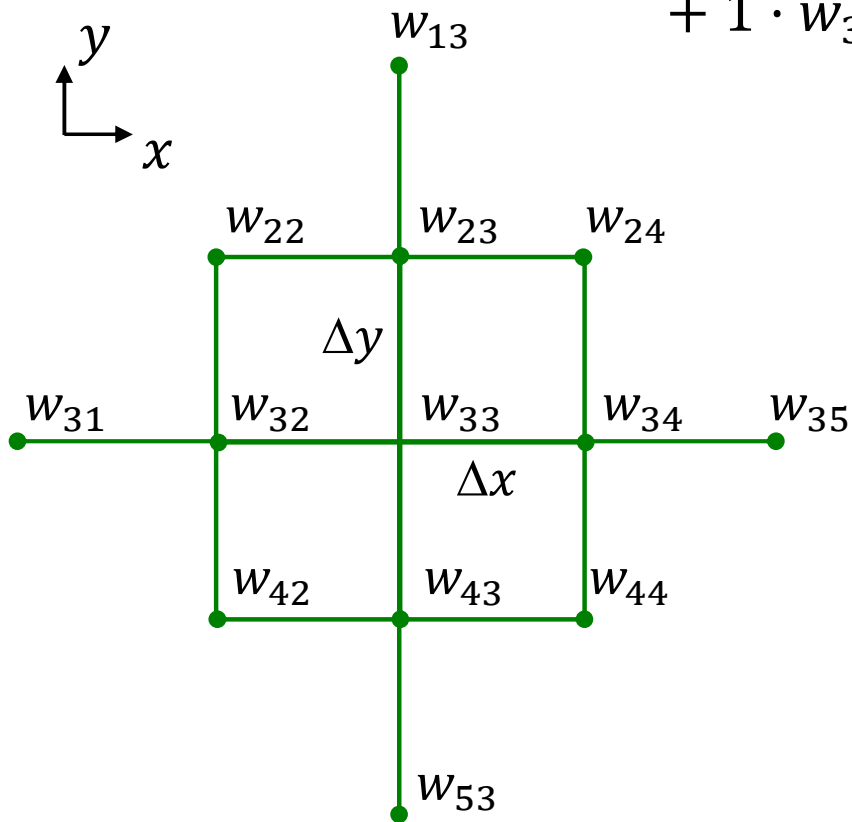


$$\begin{aligned}
 & \frac{1}{\Delta x^4} (w_{31} - 4w_{32} + 6w_{33} - 4w_{34} + w_{35}) + \\
 + & \frac{2}{\Delta x^2 \Delta y^2} (w_{22} - 2w_{23} + w_{24} - 2w_{32} + 4w_{33} - 2w_{34} + w_{42} - 2w_{43} + w_{44}) + \\
 & \frac{1}{\Delta x^4} (w_{13} - 4w_{23} + 6w_{33} - 4w_{43} + w_{53}) = \frac{12p(1-\nu^2)}{Et^3}
 \end{aligned}$$



$$\Delta x = \Delta y = \frac{L}{8}$$

$$\begin{aligned} & (w_{31} - 4w_{32} + 6w_{33} - 4w_{34} + w_{35}) + \\ & + 2(w_{22} - 2w_{23} + w_{24} - 2w_{32} + 4w_{33} - 2w_{34} + w_{42} - 2w_{43} + w_{44}) + \\ & + (w_{13} - 4w_{23} + 6w_{33} - 4w_{43} + w_{53}) = \\ & = \frac{12p(1 - \nu^2)L^4}{4096Et^3} \end{aligned}$$

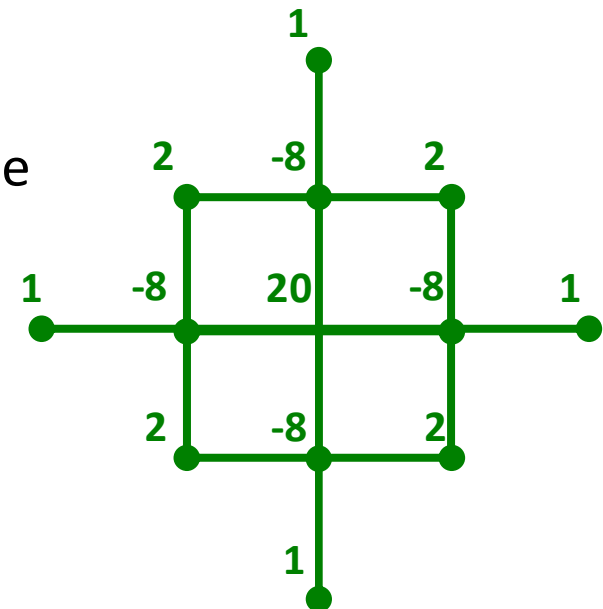


$$\Delta x = \Delta y = \frac{L}{8}$$

$$\begin{aligned}
 & 1 \cdot w_{13} + \\
 & + 2 \cdot w_{22} - 8 \cdot w_{23} + 2 \cdot w_{24} + \\
 & + 1 \cdot w_{31} - 8 \cdot w_{32} + 20 \cdot w_{33} - 8 \cdot w_{34} + 1 \cdot w_{35} + \\
 & + 2 \cdot w_{42} - 8 \cdot w_{43} + 2 \cdot w_{44} + \\
 & + 1 \cdot w_{53}
 \end{aligned}$$

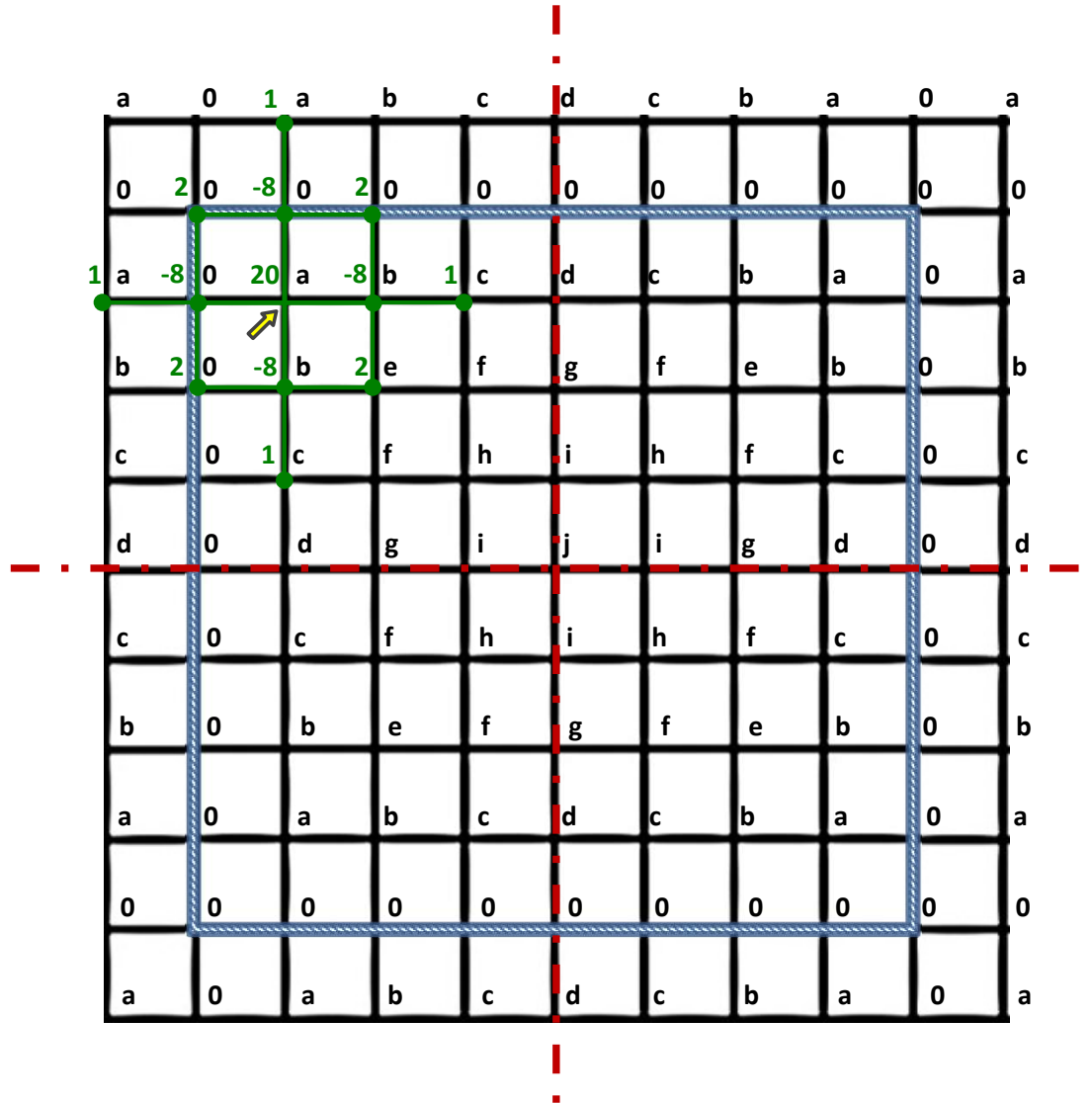
$$= \frac{12p(1 - \nu^2)L^4}{4096Et^3}$$

Differential scheme



$$1 \cdot a + 2 \cdot 0 - 8 \cdot 0 + 2 \cdot 0 + 1 \cdot a - 8 \cdot 0 + 20 \cdot a - 8 \cdot b + 1 \cdot c + 2 \cdot 0 - 8 \cdot b + 2 \cdot e + 1 \cdot c = \frac{12p(1-\nu^2)L^4}{4096Et^3}$$

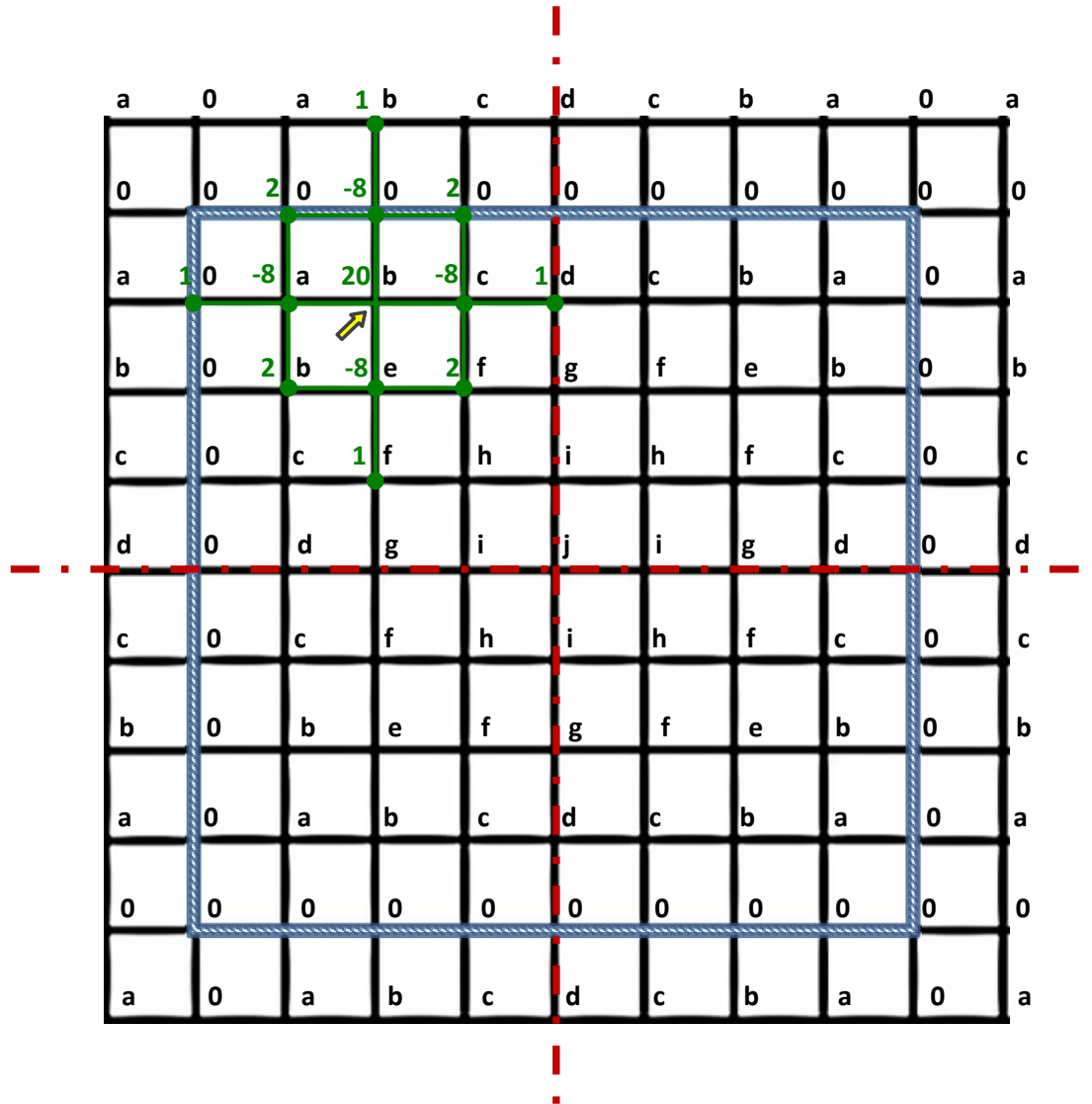
$$22 \cdot a - 16 \cdot b + 2 \cdot c + 0 \cdot d + 2 \cdot e + 0 \cdot f + 0 \cdot g + 0 \cdot h + 0 \cdot i + 0 \cdot j = \frac{12p(1-\nu^2)L^4}{4096Et^3}$$



clamped edges

$$1 \cdot b + 2 \cdot 0 - 8 \cdot 0 + 2 \cdot 0 + 1 \cdot 0 - 8 \cdot a + 20 \cdot b - 8 \cdot c + 1 \cdot d + 2 \cdot b - 8 \cdot e + 2 \cdot f + 1 \cdot f = \frac{12 (1-\nu^2)L^4}{4096Et^3}$$

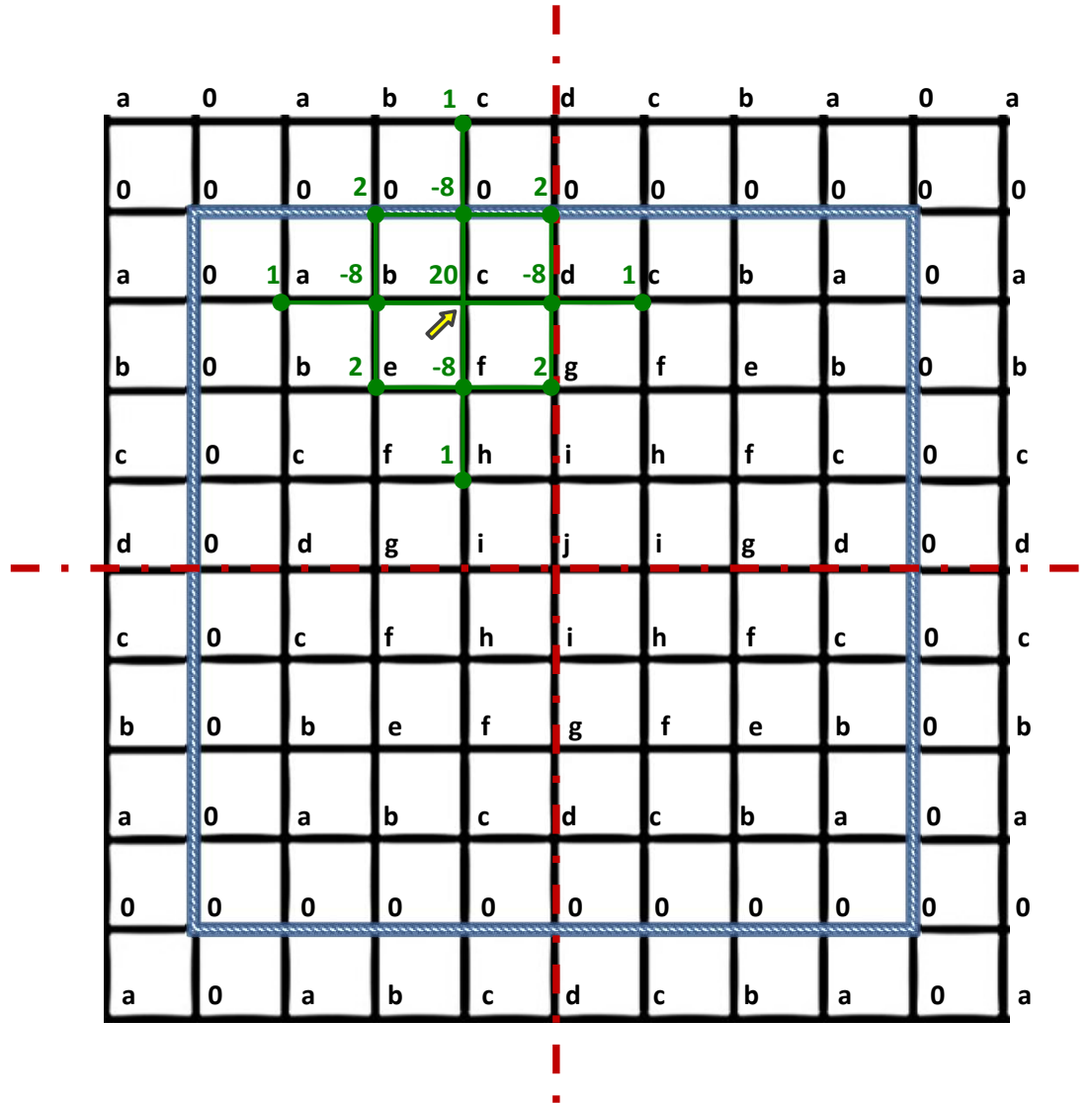
$$-8 \cdot a + 23 \cdot b - 8 \cdot c + 1 \cdot d - 8 \cdot e + 3 \cdot f + 0 \cdot g + 0 \cdot h + 0 \cdot i + 0 \cdot j = \frac{12 (1-\nu^2)L^4}{4096Et^3}$$



 clamped edges

$$1 \cdot c + 2 \cdot 0 - 8 \cdot 0 + 2 \cdot 0 + 1 \cdot a - 8 \cdot b + 20 \cdot c - 8 \cdot d + 1 \cdot c + 2 \cdot e - 8 \cdot f + 2 \cdot g + 1 \cdot h = \frac{12p(1-\nu^2)L^4}{4096 \cdot 3}$$

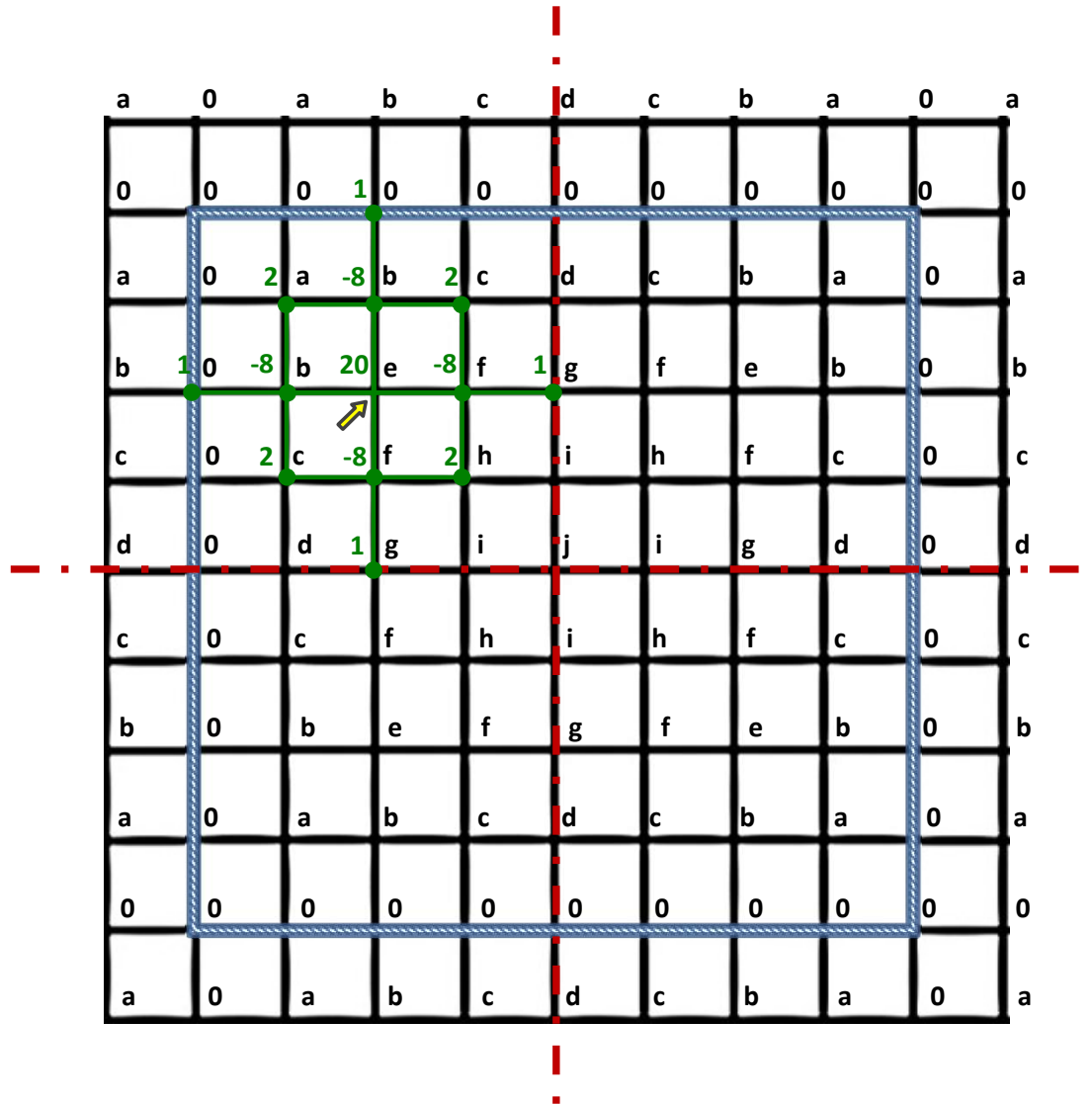
$$1 \cdot a - 8 \cdot b + 22 \cdot c - 8 \cdot d + 2 \cdot e - 8 \cdot f + 2 \cdot g + 1 \cdot h + 0 \cdot i + 0 \cdot j = \frac{12p(1-\nu^2)L^4}{4096 \cdot 3}$$



clamped edges

$$1 \cdot 0 + 2 \cdot a - 8 \cdot b + 2 \cdot c + 1 \cdot 0 - 8 \cdot b + 20 \cdot e - 8 \cdot f + 1 \cdot g + 2 \cdot c - 8 \cdot f + 2 \cdot h + 1 \cdot g = \frac{12p(1-\nu^2)L^4}{4096Et^3}$$

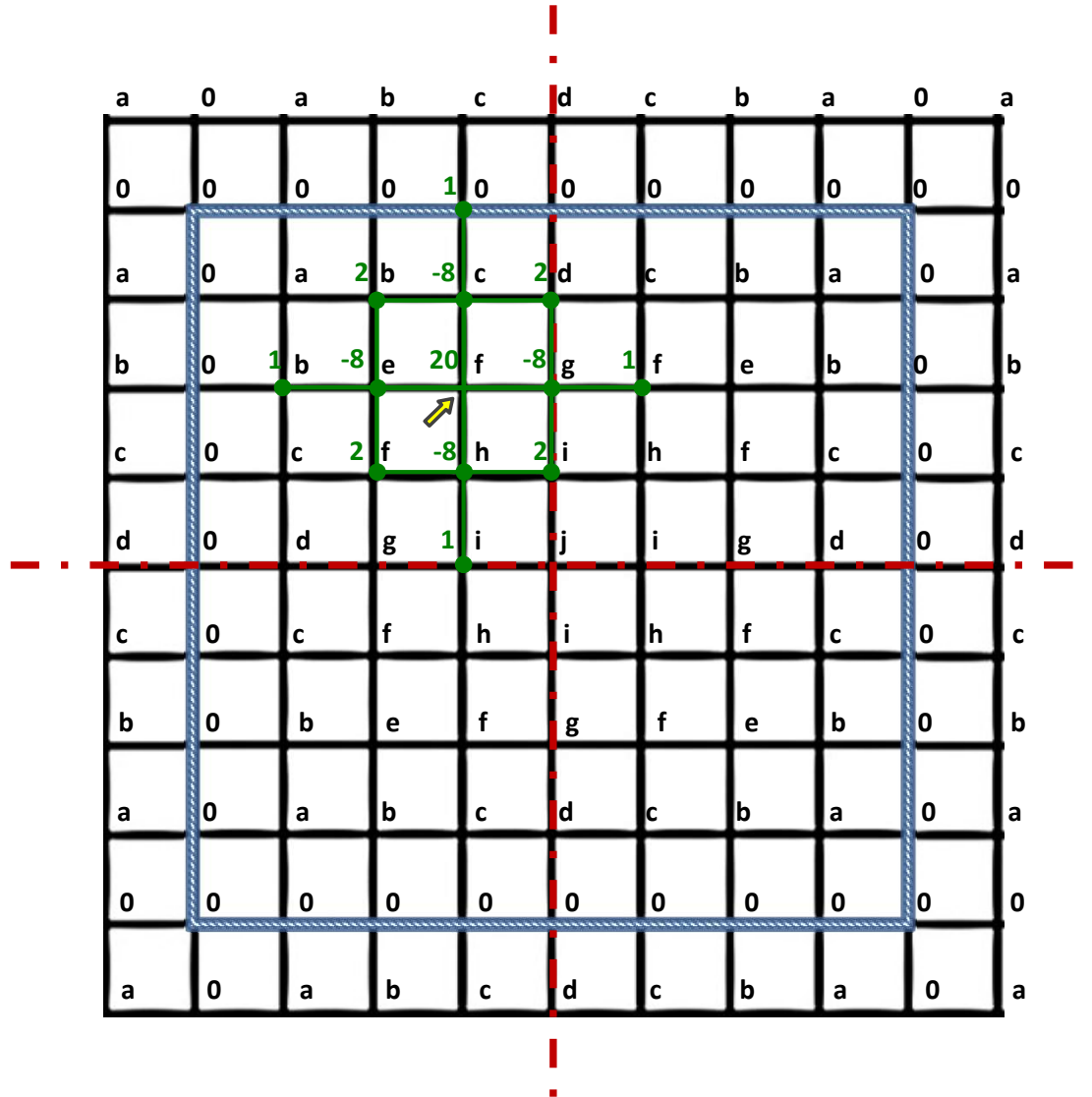
$$2 \cdot a - 16 \cdot b + 4 \cdot c + 0 \cdot d + 20 \cdot e - 16 \cdot f + 2 \cdot g + 2 \cdot h + 0 \cdot i + 0 \cdot j = \frac{12p(1-\nu^2)L^4}{4096Et^3}$$



clamped edges

$$1 \cdot 0 + 2 \cdot b - 8 \cdot c + 2 \cdot d + 1 \cdot b - 8 \cdot e + 20 \cdot f - 8 \cdot g + 1 \cdot f + 2 \cdot f - 8 \cdot h + 2 \cdot i + 1 \cdot i = \frac{12p(1-\nu^2)L^4}{4096 \cdot 3}$$

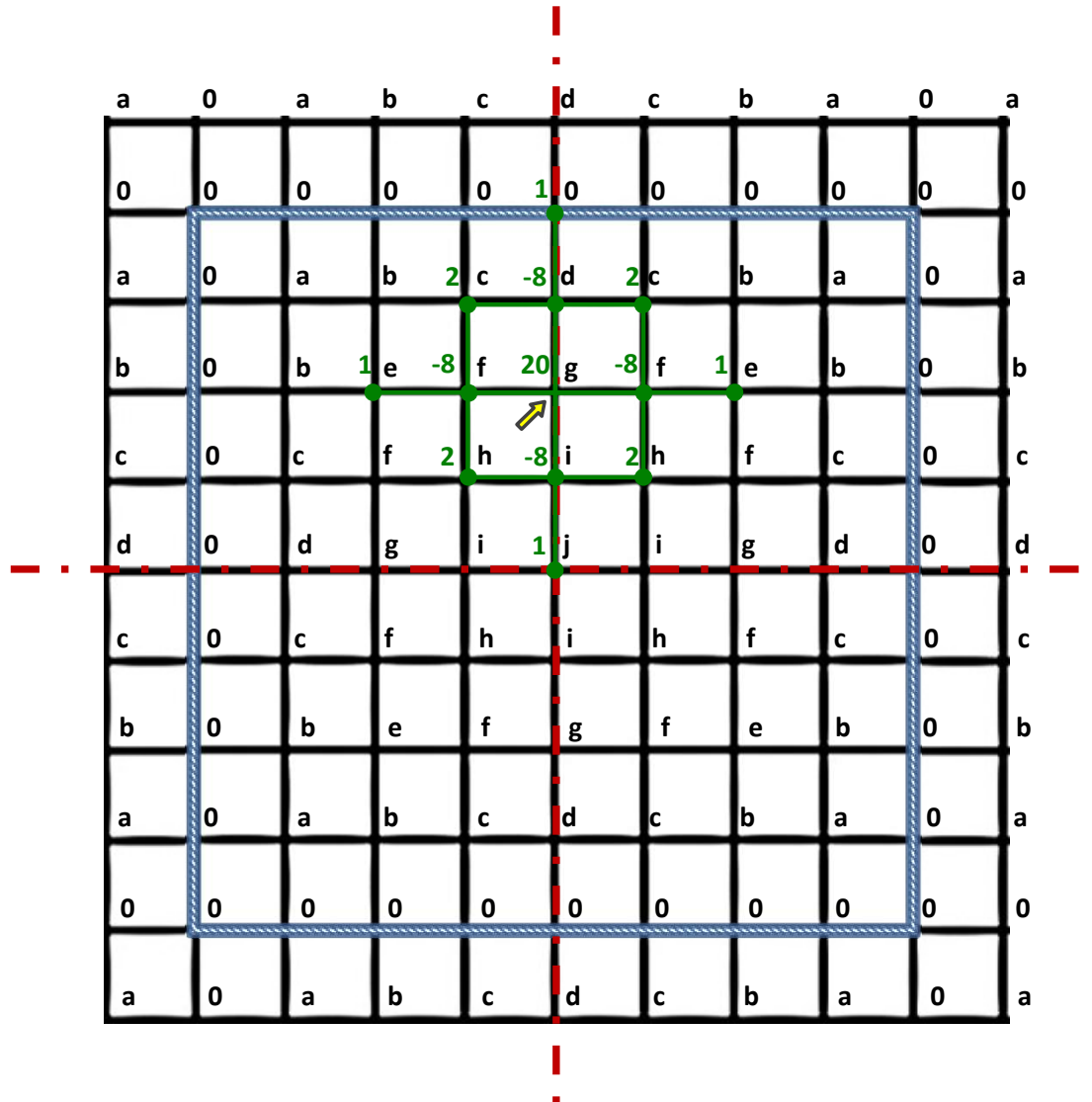
$$0 \cdot a + 3 \cdot b - 8 \cdot c + 2 \cdot d - 8 \cdot e + 23 \cdot f - 8 \cdot g - 8 \cdot h + 3 \cdot i + 0 \cdot j = \frac{12p(1-\nu^2)L^4}{4096 \cdot 3}$$



 clamped edges

$$1 \cdot 0 + 2 \cdot c - 8 \cdot d + 2 \cdot c + 1 \cdot e - 8 \cdot f + 20 \cdot g - 8 \cdot f + 1 \cdot e + 2 \cdot h - 8 \cdot i + 2 \cdot h + 1 \cdot j = \frac{12p(1-\nu^2)L^4}{4096Et^3}$$

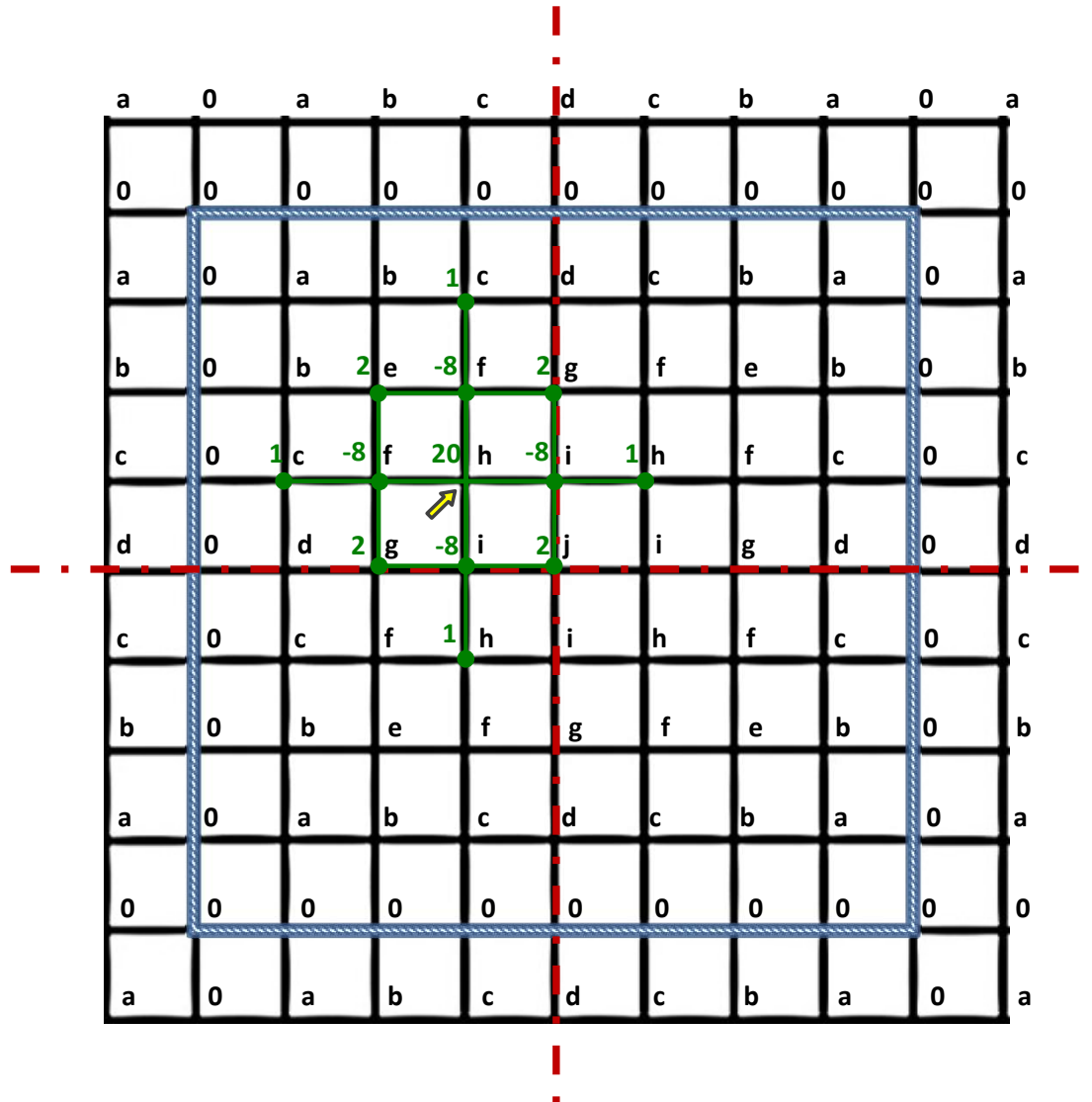
$$0 \cdot a + 0 \cdot b + 4 \cdot c - 8 \cdot d + 2 \cdot e - 16 \cdot f + 20 \cdot g + 4 \cdot h - 8 \cdot i + 1 \cdot j = \frac{12(1-\nu^2)L^4}{4096Et^3}$$



 clamped edges

$$1 \cdot c + 2 \cdot e - 8 \cdot f + 2 \cdot g + 1 \cdot c - 8 \cdot f + 20 \cdot h - 8 \cdot i + 1 \cdot h + 2 \cdot g - 8 \cdot i + 2 \cdot j + 1 \cdot h = \frac{12(1-\nu^2)L^4}{4096^3}$$

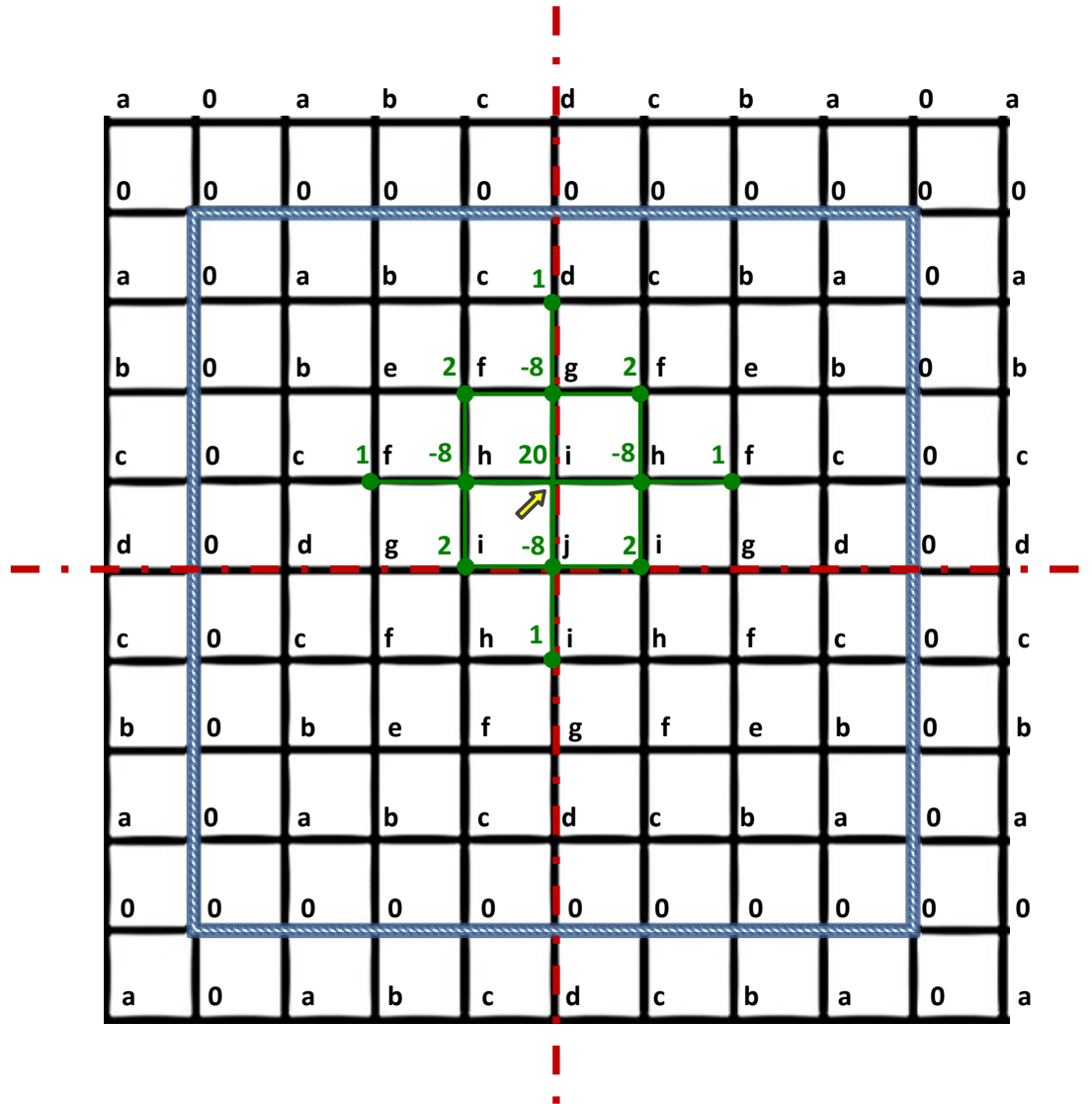
$$0 \cdot a + 0 \cdot b + 2 \cdot c + 0 \cdot d + 2 \cdot e - 16 \cdot f + 4 \cdot g + 22 \cdot h - 16 \cdot i + 2 \cdot j = \frac{12p(1-\nu^2)L^4}{4096^3}$$



clamped edges

$$1 \cdot d + 2 \cdot f - 8 \cdot g + 2 \cdot f + 1 \cdot f - 8 \cdot h + 20 \cdot i - 8 \cdot h + 1 \cdot f + 2 \cdot i - 8 \cdot j + 2 \cdot i + 1 \cdot i = \frac{12p(1-\nu^2)L^4}{4096 \cdot 3}$$

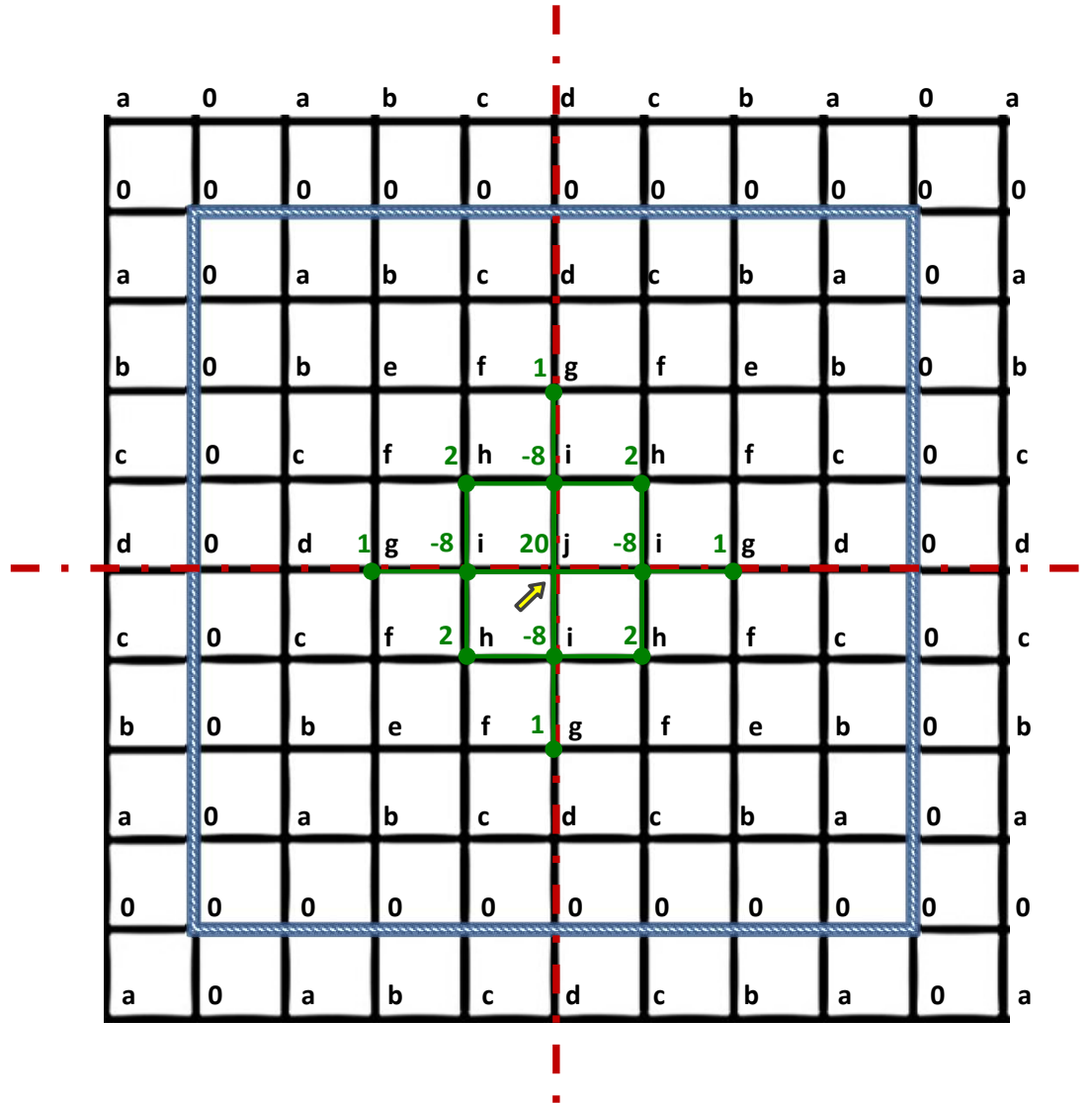
$$0 \cdot a + 0 \cdot b + 0 \cdot c + 1 \cdot d + 0 \cdot e + 6 \cdot f - 8 \cdot g - 16 \cdot h + 25 \cdot i - 8 \cdot j = \frac{12p(1-\nu^2)L^4}{4096 \cdot 3}$$



clamped edges

$$1 \cdot g + 2 \cdot h - 8 \cdot i + 2 \cdot h + 1 \cdot g - 8 \cdot i + 20 \cdot j - 8 \cdot i + 1 \cdot g + 2 \cdot h - 8 \cdot i + 2 \cdot h + 1 \cdot g = \frac{12p(1-\nu^2)L^4}{4096Et^3}$$

$$0 \cdot a + 0 \cdot b + 0 \cdot c + 0 \cdot d + 0 \cdot e + 0 \cdot f + 4 \cdot g + 8 \cdot h - 32 \cdot i + 20 \cdot j = \frac{12(1-\nu^2)L^4}{4096Et^3}$$



 clamped edges

$$22 \cdot a - 16 \cdot b + 2 \cdot c + 0 \cdot d + 2 \cdot e + 0 \cdot f + 0 \cdot g + 0 \cdot h + 0 \cdot i + 0 \cdot j = \frac{12(1-\nu^2)L^4}{4096Et^3}$$

$$-8 \cdot a + 23 \cdot b - 8 \cdot c + 1 \cdot d - 8 \cdot e + 3 \cdot f + 0 \cdot g + 0 \cdot h + 0 \cdot i + 0 \cdot j = \frac{12p(1-\nu^2)L^4}{4096Et^3}$$

$$1 \cdot a - 8 \cdot b + 22 \cdot c - 8 \cdot d + 2 \cdot e - 8 \cdot f + 2 \cdot g + 1 \cdot h + 0 \cdot i + 0 \cdot j = \frac{12p(1-\nu^2)L^4}{4096Et^3}$$

$$0 \cdot a + 2 \cdot b - 16 \cdot c + 21 \cdot d + 0 \cdot e + 4 \cdot f - 8 \cdot g + 0 \cdot h + 1 \cdot i + 0 \cdot j = \frac{12p(1-\nu^2)L^4}{4096^3}$$

$$2 \cdot a - 16 \cdot b + 4 \cdot c + 0 \cdot d + 20 \cdot e - 16 \cdot f + 2 \cdot g + 2 \cdot h + 0 \cdot i + 0 \cdot j = \frac{12p(1-\nu^2)L^4}{4096E^3}$$

$$0 \cdot a + 3 \cdot b - 8 \cdot c + 2 \cdot d - 8 \cdot e + 23 \cdot f - 8 \cdot g - 8 \cdot h + 3 \cdot i + 0 \cdot j = \frac{12p(1-\nu^2)L^4}{4096Et^3}$$

$$0 \cdot a + 0 \cdot b + 4 \cdot c - 8 \cdot d + 2 \cdot e - 16 \cdot f + 20 \cdot g + 4 \cdot h - 8 \cdot i + 1 \cdot j = \frac{12(1-\nu^2)L^4}{4096^3}$$

$$0 \cdot a + 0 \cdot b + 2 \cdot c + 0 \cdot d + 2 \cdot e - 16 \cdot f + 4 \cdot g + 22 \cdot h - 16 \cdot i + 2 \cdot j = \frac{12p(1-\nu^2)L^4}{4096^3}$$

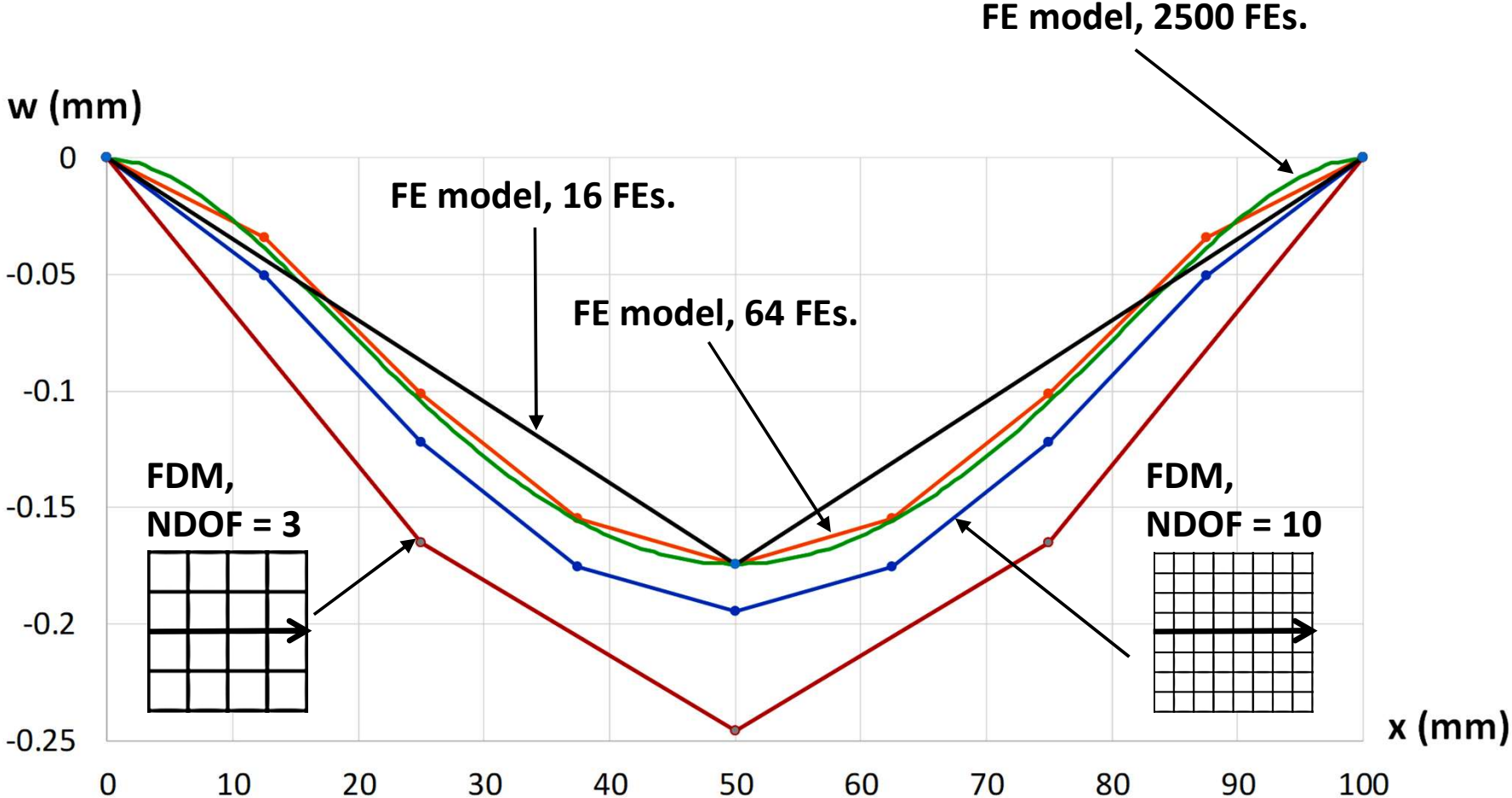
$$0 \cdot a + 0 \cdot b + 0 \cdot c + 1 \cdot d + 0 \cdot e + 6 \cdot f - 8 \cdot g - 16 \cdot h + 25 \cdot i - 8 \cdot j = \frac{12p(1-\nu^2)L^4}{4096Et^3}$$

$$0 \cdot a + 0 \cdot b + 0 \cdot c + 0 \cdot d + 0 \cdot e + 0 \cdot f + 4 \cdot g + 8 \cdot h - 32 \cdot i + 20 \cdot j = \frac{12p(1-\nu^2)L^4}{4096Et^3}$$

$$\begin{bmatrix}
 22 & -16 & 2 & 0 & 2 & 0 & 0 & 0 & 0 & 0 \\
 -8 & 23 & -8 & 1 & -8 & 3 & 0 & 0 & 0 & 0 \\
 1 & -8 & 22 & -8 & 2 & -8 & 2 & 1 & 0 & 0 \\
 0 & 2 & -16 & 21 & 0 & 4 & -8 & 0 & 1 & 0 \\
 2 & -16 & 4 & 0 & 20 & -16 & 2 & 2 & 0 & 0 \\
 0 & 3 & -8 & 2 & -8 & 23 & -8 & -8 & 3 & 0 \\
 0 & 0 & 4 & -8 & 2 & -16 & 20 & 4 & -8 & 1 \\
 0 & 0 & 2 & 0 & 2 & -16 & 4 & 22 & -16 & 2 \\
 0 & 0 & 0 & 1 & 0 & 6 & -8 & -16 & 25 & -8 \\
 0 & 0 & 0 & 0 & 0 & 0 & 4 & 8 & -32 & 20
 \end{bmatrix}
 \begin{Bmatrix}
 a \\
 b \\
 c \\
 d \\
 e \\
 f \\
 g \\
 h \\
 i \\
 j
 \end{Bmatrix}
 = \frac{12p(1 - \nu^2)L^4}{4096Et^3}
 \begin{Bmatrix}
 1 \\
 1 \\
 1 \\
 1 \\
 1 \\
 1 \\
 1 \\
 1 \\
 1 \\
 1
 \end{Bmatrix}$$

Point	a	b	c	d	e	f	g	h	i	j
w (mm)	-0.014	-0.033	-0.046	-0.051	-0.077	-0.110	-0.122	-0.158	-0.175	-0.194

Deformation of a square plate: Finite Difference Method and FEM solution (4 node SHELL 181)



Bending moments

$$m_x = -\frac{Et^3}{12(1-\nu^2)} \left(\frac{\partial^2 w}{\partial x^2} + \nu \frac{\partial^2 w}{\partial y^2} \right)$$

$$m_y = -\frac{Et^3}{12(1-\nu^2)} \left(\frac{\partial^2 w}{\partial y^2} + \nu \frac{\partial^2 w}{\partial x^2} \right)$$

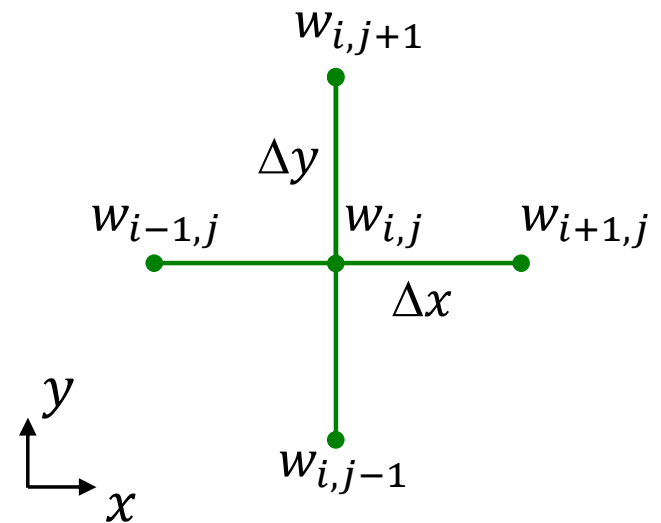
Normal stress components on the top layer ($z = \frac{1}{2}t$)

$$\sigma_x = \frac{6m_x}{t^2} \quad ; \quad \sigma_y = \frac{6m_y}{t^2}$$

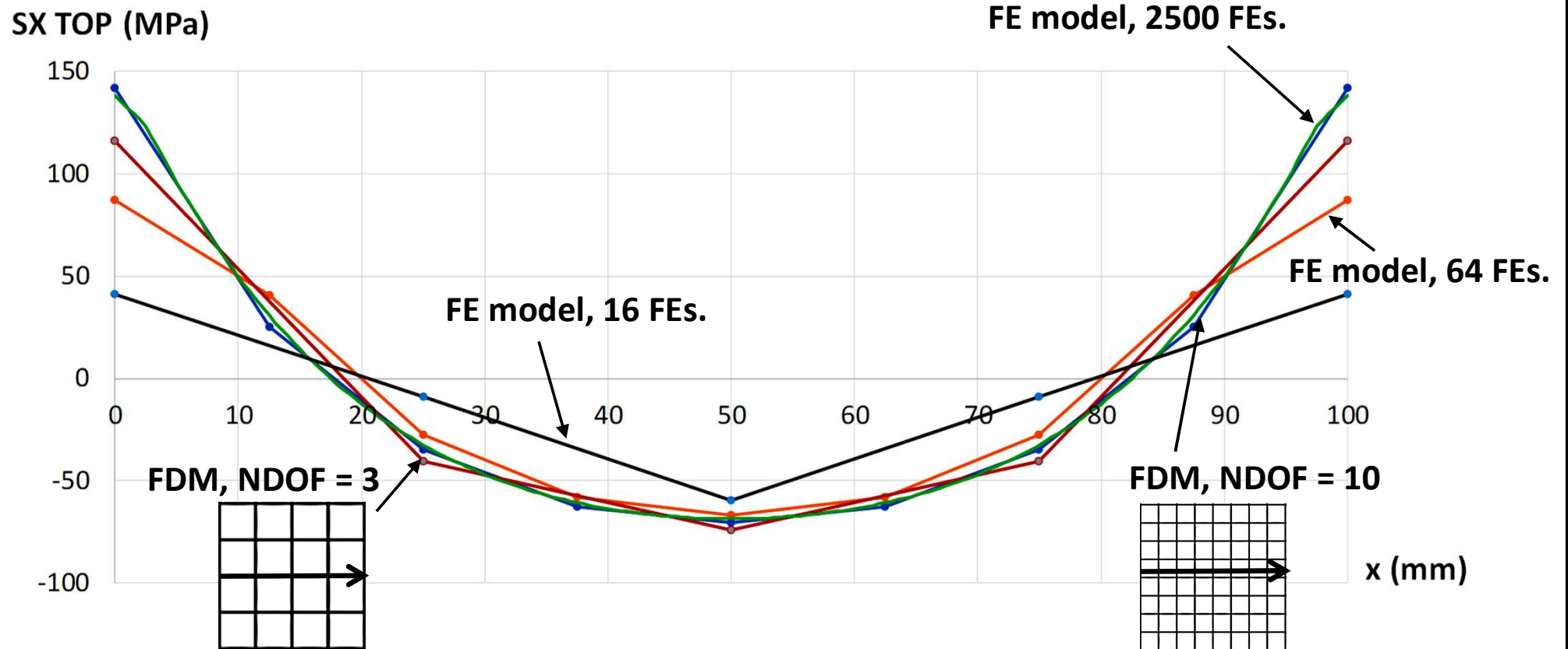
Curvatures:

$$\frac{\partial^2 w}{\partial x^2} = \frac{w_{i+1,j} - 2w_{i,j} + w_{i-1,j}}{\Delta x^2}$$

$$\frac{\partial^2 w}{\partial y^2} = \frac{w_{i,j+1} - 2w_{i,j} + w_{i,j-1}}{\Delta y^2}$$



Stress SX component on the top layer: Finite Difference Method and FEM solution (4 node SHELL 181)



Stress SY component on the top layer: Finite Difference Method and FEM solution (4 node SHELL 181)

